

If-less KPP

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- Why KPP?

- ...don't ask.

- Why if-less?

- if-switches may cause:

- discontinuities of second derivative

- discontinuities of first derivative

- discontinuities of function

- **hysteresis** and **multiple** solutions

- To what extend if-less?

- ...identify and eliminate the most offending ones

- ...this is a data-assimilation workshop.

KPP boundary layer model:

Extent of PBL h_{bl} is determined from bulk Richardson number (LMD94)

$$Ri_b(z) = \frac{\Delta z g [\rho(z) - \rho_r] / \rho_0}{|\mathbf{u}_r - \mathbf{u}(z)|^2 + V_t^2(z)} \quad Ri_b(-h_{bl}) = Ri_{cr} = 0.3$$

after which h_{bl} is checked against Monin-Obukhov $h_{MO} = u_*^3 / (\kappa \cdot B_f)$, and Ekman $h_{Ek} = 0.7 u_* / f$ depth and limited by both of them in the case of stable buoyancy forcing $B_f > 0$.

Once h_{bl} is known $K_{m,s}(z) = w_{m,s} \cdot h_{bl} \cdot G(z/h_{bl})$ where $G(.)$ is universal non-dimensional shape function and $w_{m,s} = \kappa u_* \cdot \psi_{m,s}(z B_f / u_*^3)$.

- relies on Monin-Obukhov similarity theory
- KPP a bulk, non-local model of intermediate complexity
- a quasi-equilibrium, diagnostic model
- multi-process model
- widely used (CCM, POP, MIT, OPA); mostly for climate modeling

Evolution of KPP: Summary of changes in KPP since 1994
by W. Large and G. Danabasoglu (2003), (2005):

- Turbulent velocity scale limit in **stable** regime
- Diurnal cycle in SW Rad. heat flux
- Critical bulk Ri depends on vertical resolution
- C_v depends on BVF
- Correct Ekman and Monin-Obukhov depth limit computations
- Compute interior convection **after** BL mixing is done
- Modify usage of N in turbulent shear computation
- Quadratic interpolation of Ri to find h_{bl}
- Monin-Obukhov depth limit is considered for elimination

Motivation

Early ROMS solution exhibit biases in thermocline depth

- too shallow in most cases

Overall excessively sensitive to numerical discretization

- h_{bl} fields are too noisy
- resolution drift: h_{bl} tends to go deeper with grid refinement

Sources of discontinuous behavior:

- $Ri_b(z)$ oscillates if $\mathbf{u}(z)$ is Ekman spiral (prevented only by h_{EK} -limit)
- hysteresis h_{MO} limitation logic
- hysteresis h_{EK} limitation logic
- vertical grid-point locking

Integral formulation of PBL

- $Ri_b(z)$ disregards velocity profile and 3D-nality within PBL

Calibration and tuning

- parameterization of elementary processes
- 1D experience
- 3D experience

Criterion for finding h_{bl} : We define surface PBL as an integral layer within which net production of turbulence due to shear-layer instability is balanced by dissipation due to stratification,

$$Cr(z) = \int_z^{\text{surface}} \mathcal{K}(z) \left\{ \left| \frac{\partial \mathbf{u}}{\partial z} \right|^2 - \frac{N^2}{\text{Ri}_{cr}} - C_{Ek} \cdot f^2 \right\} dz' + \frac{V_t^2(z)}{z}$$

and search for crossing point $Cr(z) = 0$.

$$N^2 = -\frac{g}{\rho_0} \cdot \frac{\partial \rho}{\partial z} \Big|_{ad} \quad \text{is B-V frequency (} ad \equiv \text{adiabatic)};$$

f is Coriolis parameter; C_{Ek} is a nondimensional constant;

$V_t^2(z)$ is unresolved turbulent velocity shear (same as in LMD94);

Integration Kernel $\mathcal{K}(z) = \frac{\zeta - z}{\epsilon h_{bl} + \zeta - z}$ is to ignore contribution from

near-surface sublayer ϵh_{bl} where M-O similarity law is not valid (plays the same role as to distinguish between ρ_{ref} vs. ρ_{surf} in Ri_b of LMD94). ζ is free surface; $\epsilon = 0.1$.

- Same result as Ri_b the case of linear velocity profile, but otherwise

$$\int_{z'}^{z''} \left| \frac{\partial \mathbf{u}}{\partial z} \right|^2 dz \geq \frac{|\mathbf{u}'' - \mathbf{u}'|^2}{z'' - z'}$$

- $Cr(z)$ is **monotonic** for Ekman spiral \Rightarrow no sudden jumps of h_{bl}
- Numerically more attractive, since $\mathbf{u}(z)$ and $\rho(z)$ can be reconstructed as continuous functions
- Avoids introduction of *reference* potential density: basically integration Brunt-Väisälä frequency. Allows formalism of *adiabatic* derivatives and differences to achieve monotonicity
- Correct account for thermobaric effect: Bill Large: to determine extent of BL one must bring water parcel **from reference depth to** $z = -h_{bl}$ and compare its density with the ambient fluid **there**. We never did it this way in ROMS community (?)
- Avoids ambiguity for merging top and bottom BLs

Pure physical limits:

destabilizing vs. stabilizing effects:

- balance $\left| \frac{\partial \mathbf{u}}{\partial z} \right|^2$ vs. $\frac{N^2}{\text{Ri}_{\text{cr}}} \Rightarrow$ shear layer instability
- $\left| \frac{\partial \mathbf{u}}{\partial z} \right|^2$ vs. $C_{\text{Ek}} \cdot f^2 \Rightarrow$ turbulent Ekman layer
- *negatively* forced $\frac{N^2}{\text{Ri}_{\text{cr}}}$ vs. $V_t^2 \Rightarrow$ free convection

Monin-Obukhov depth limit $h_{bl} \leq h_{MO} = \frac{C^{MO} \cdot u_*^3}{\kappa \cdot B_f}$ if $B_f(z) > 0$.

Because of solar radiation absorption, buoyancy forcing $B_f = B_f(z)$ increases with depth, possibly changing sign *from unstable to stable*
 \Rightarrow a case when $B_f(-\text{overestimated } h_{bl}) > 0$, but $B_f(-h_{MO}) < 0 \Rightarrow$
hysteresis and oscillations in h_{bl}

solution # 1: (2003) use $B_f = B_f(-h_{MO})$ in computation of h_{MO} , i.e. implicit search for k enclosing z^* , such that

$$z_k \leq z^* \leq z_{k+1} \quad \text{and} \quad h_{MO}(z_k) \leq |z^*| \leq h_{MO}(z_{k+1})$$

then solve

$$\frac{h_{MOk}(z_{k+1} - z^*) + h_{MOk+1}(z^* - z_k)}{z_{k+1} - z_k} + z^* = 0$$

resulting in

$$h_{MO} = -z^* = \frac{\frac{C^{MO} u_*^3}{\kappa} (B_{f'k+1} z_{k+1} - B_{f'k} z_k)}{B_{f'k+1} B_{f'k} (z_{k+1} - z_k) + \frac{C^{MO} u_*^3}{\kappa} (B_{f'k} - B_{f'k+1})}$$

above $B_f' = \max(B_f, 0)$; if k not found \Rightarrow no limit; **no singularity** if either $B_f \rightarrow 0$;
 limit applied **outside** $B_f > 0$ **logic**: it is already taken into account in computing h_{MO} ;
since h_{bl} **is not involved** \Rightarrow **no possibility of hysteresis**

solution # 2: (2005) Eliminate M-O limit altogether.

Ekman depth limitation: $h_{bl} \leq h_{Ek} = 0.7u_*/f$ for *stable* boundary layer; should be $h_{bl} = h_{Ek}$ for *neutral* forcing and stratification

Length $\mathcal{L} = u_*/f$ and velocity $\mathcal{U} = u_*$ are natural scaling parameters for neutrally stratified problem

$$i \cdot f \mathbf{u} = \frac{\partial}{\partial z} \left(w_m |z| \frac{\partial \mathbf{u}}{\partial z} \right)$$

where $\mathbf{u} = u + iv$, and $w_m \equiv \kappa u_*$, and κ is von Karman constant.

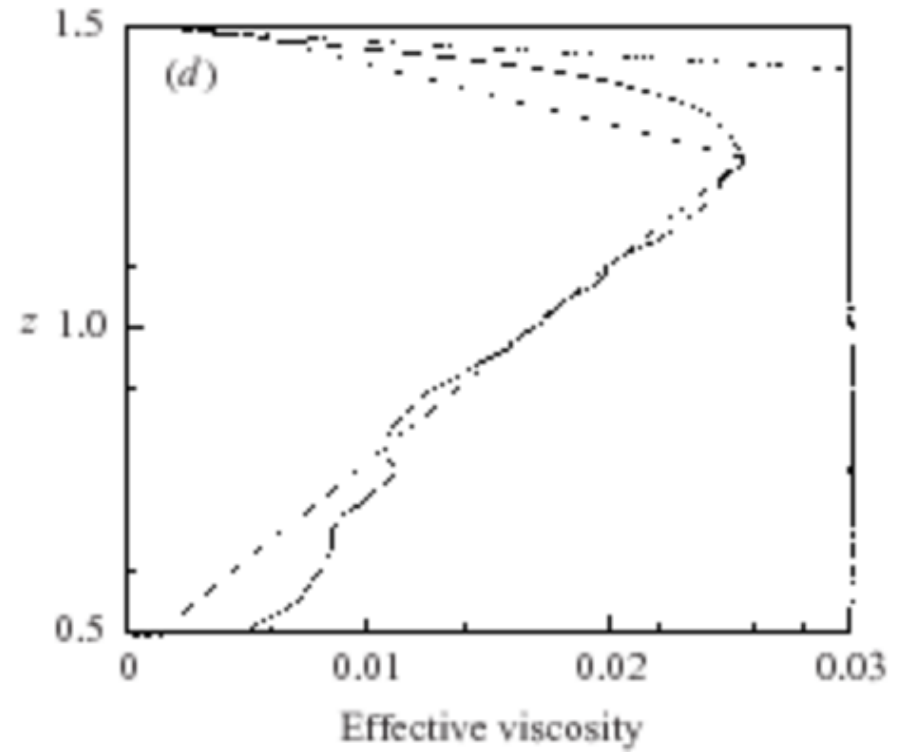
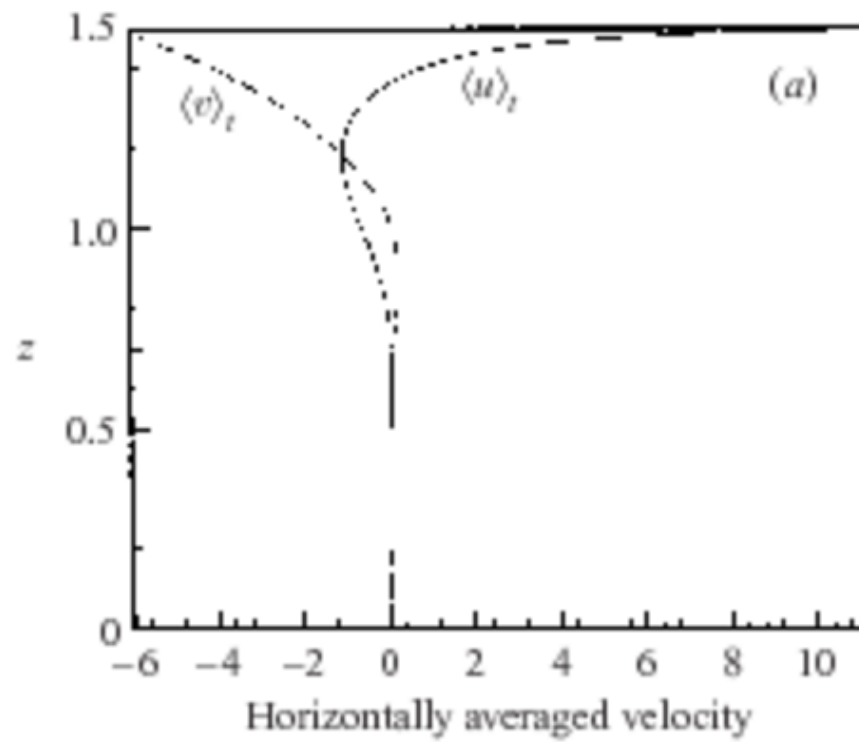
- Most vertical mixing schemes are "Coriolis-blind".
- Coriolis effect plays no role in determining h_{bl} via bulk Ri criterion; h_{Ek} -limit is applied *a'posterio*ri, and only for stable buoyancy forcing.
- Because of light absorption, stability increases downward resulting in hysteresis if $B_f(\text{unlimited } h_{bl}) > 0$, but $B_f(h_{Ek}) < 0$ which is manifested by h_{bl} oscillations and jumps

??? integrate h_{Ek} -limit into KPP BL criterion, balance

$$\int \left| \frac{\partial \mathbf{u}}{\partial z} \right|^2 dz' \quad \text{vs.} \quad \int f^2 dz' \quad ???$$

DNS and LES simulations of Turbulent Ekman Layer:

- Zikanov, O., D. N. Slinn, and M. R. Dhanak, 2003: Large-eddy simulations of the wind-induced turbulent Ekman layer. *J. Fluid. Mech.*, **495**, 343-368.
- Esau, I., 2004: Simulation of Ekman Boundary Layers by Large Eddy Model with Dynamic Mixed Sub-filter Closure. *Envir. Fluid Mech.*, **4**, 273-303, DOI: 10.1023/B:EFMC.00000024236.38450.8d
- Coleman G. N., 1999: Similarity statistics from direct numerical simulation of the neutrally stratified PBL. *J. Atmos. Sci.*, **56**, 891-900.
- Coleman G. N., J. H. Ferziger, and P. R. Spalart, 1990: A numerical study of the turbulent Ekman layer. *J. Fluid. Mech.*, **213**, 313-348.
- Parmhed, O., I. Kos, and B. Grisogono, 2005: An improved Ekman layer approximation for smooth eddy diffusivity profiles. *Boundary-Layer Meteor.*, 115(3), 399-407.



DNS simulations from, Zikanov *et al* 2003.

Modified Ekman problem: $i \cdot f \mathbf{u} = \frac{\partial}{\partial z} \left[w_m \mathcal{L} G \left(\frac{z}{\mathcal{L}} \right) \frac{\partial \mathbf{u}}{\partial z} \right]$

G is KPP non-dimensional shape function

$$G(\sigma) = |\sigma| (1 - \sigma)^2 + \begin{cases} \frac{(\sigma - \sigma_0)^2}{2\sigma_0}, & \sigma < \sigma_0 \\ 0 & \text{otherwise} \end{cases} \quad \sigma_0 = 0.1$$

B.C.: $w_m \mathcal{L} G \left(\frac{z}{\mathcal{L}} \right) \frac{\partial \mathbf{u}}{\partial z} \Big|_{z=0} = u_*^2 \mathbf{1}_\tau \quad \Rightarrow \quad \frac{\partial \mathbf{u}}{\partial z} \Big|_{z=0} = \frac{u_* \mathbf{1}_\tau}{\kappa \mathcal{L} \sigma_0 / 2}$
 $\mathbf{u} = 0$, if $z < -\mathcal{L}$

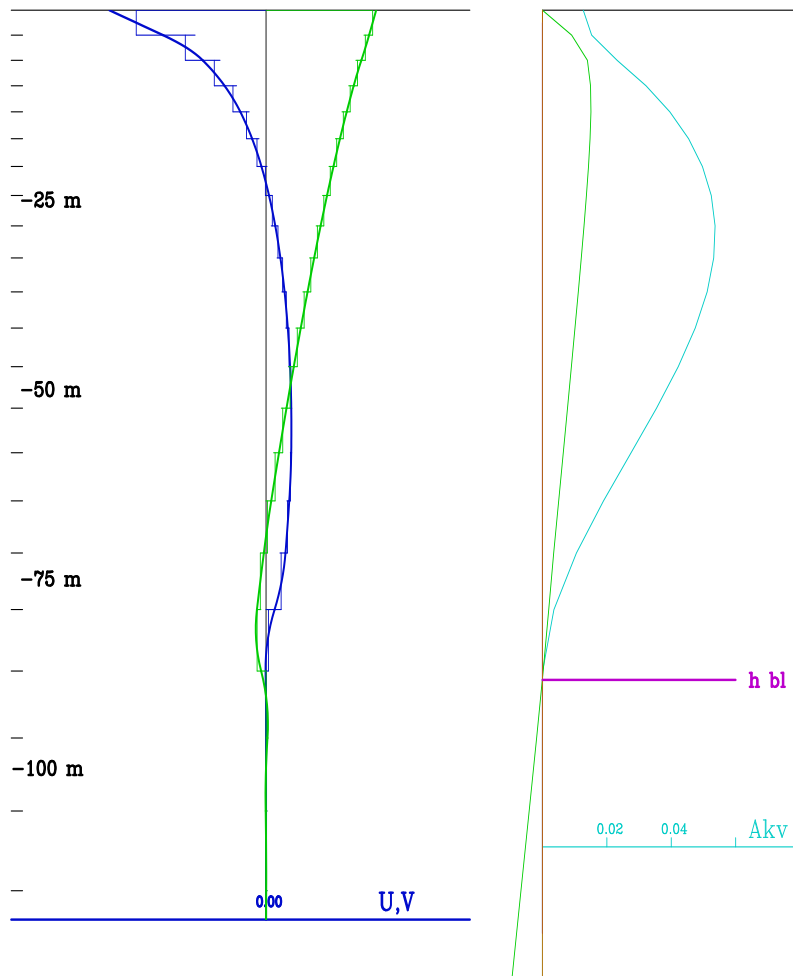
Nondimensionalization: Postulate that depth of generated this way boundary layer is equal to Ekman length and introduce scaling,

$$z = \mathcal{L} \sigma = \sigma \cdot 0.7 u_* / f \quad \mathbf{u} = u_* \cdot \tilde{\mathbf{u}},$$

hence

$$\frac{\partial}{\partial \sigma} \left(G(\sigma) \frac{\partial \tilde{\mathbf{u}}}{\partial \sigma} \right) = i \cdot \frac{\kappa}{0.7} \tilde{\mathbf{u}}, \quad \frac{\partial \tilde{\mathbf{u}}}{\partial \sigma} \Big|_{\sigma=0} = \frac{2}{\kappa \sigma_0}, \quad \tilde{\mathbf{u}} \Big|_{\sigma < -1} = 0$$

everything has been scaled out.



Recognize Coriolis force as *stabilizing* effect (balancing vertical shear production), construct

$$Cr(z) = \int_z^{\text{surf}} \mathcal{K}(z') \left\{ \left| \frac{\partial \mathbf{u}}{\partial z} \right|^2 - C_{Ek} \cdot f^2 \right\} dz'$$

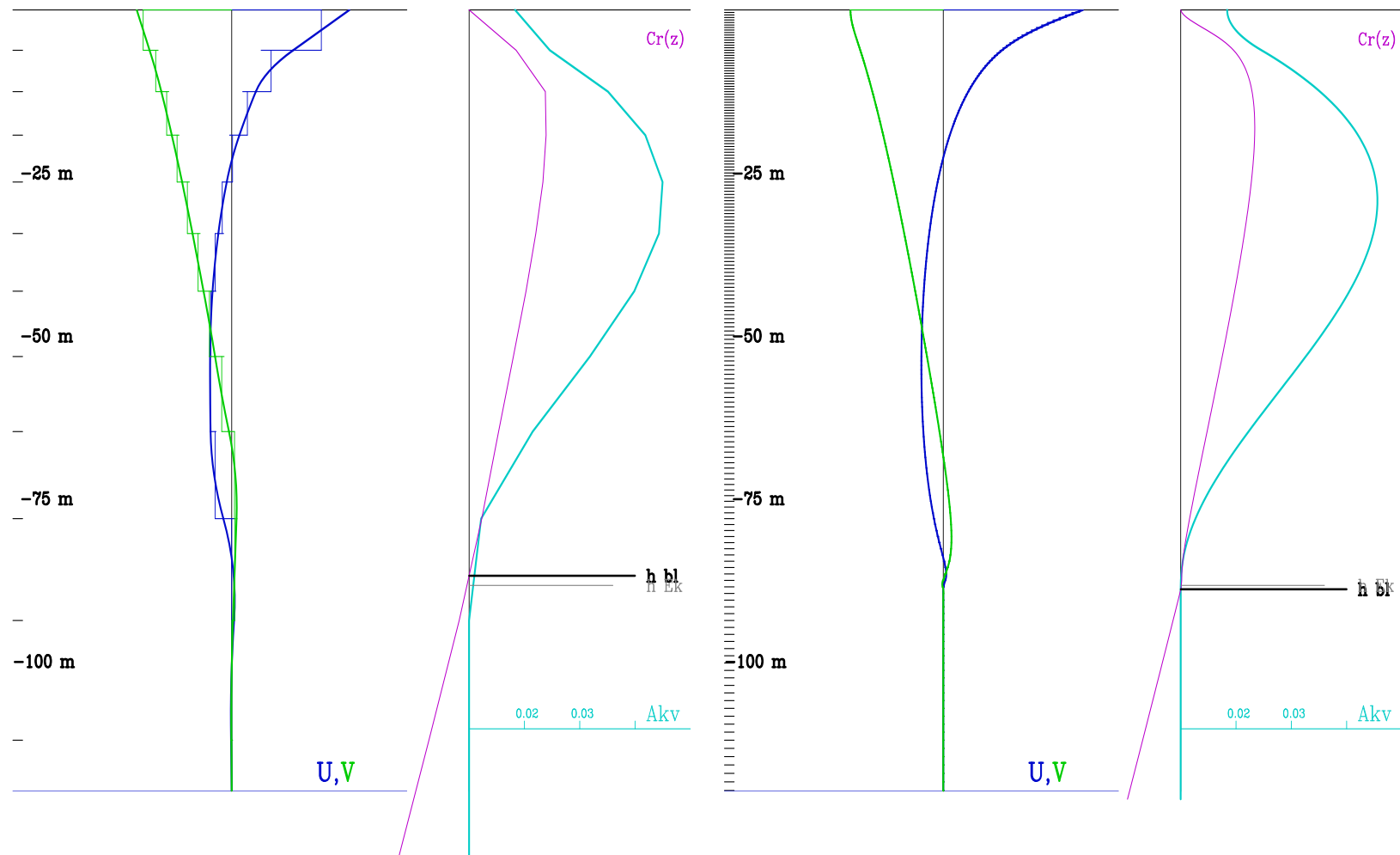
apply the same scaling

$$\widetilde{Cr}(\sigma) = \frac{1}{(0.7)^2} \int_{\sigma}^0 \mathcal{K}(\sigma) \left\{ \left| \frac{\partial \tilde{\mathbf{u}}}{\partial \sigma} \right|^2 - C_{Ek} \right\} d\sigma'$$

and demand that $\widetilde{Cr}(-1) = 0$.

$C_{Ek} = 258$ provided that

$\mathcal{K}(\sigma) = |\sigma|/(|\sigma| + \epsilon)$, where $\epsilon = 0.1$



Coarse, $N = 32$ and fine, $N = 512$ resolution. h_{EK} is shown for reference only and does not participate in determining h_{bI} .

- **presence of $\mathcal{K}(\sigma)$ is essential for convergence**
- **overall extremely robust**

Numerical Issues

velocities are smooth across $z = -h_{\text{bl}}$, **but tracers are not**

Computation of Ri_b/Cr at vertical ρ vs. W -points:

- ρ -placement is natural for finite-difference (trapezoidal-rule) terms in Ri_b/Cr (but not for V_t^2), however

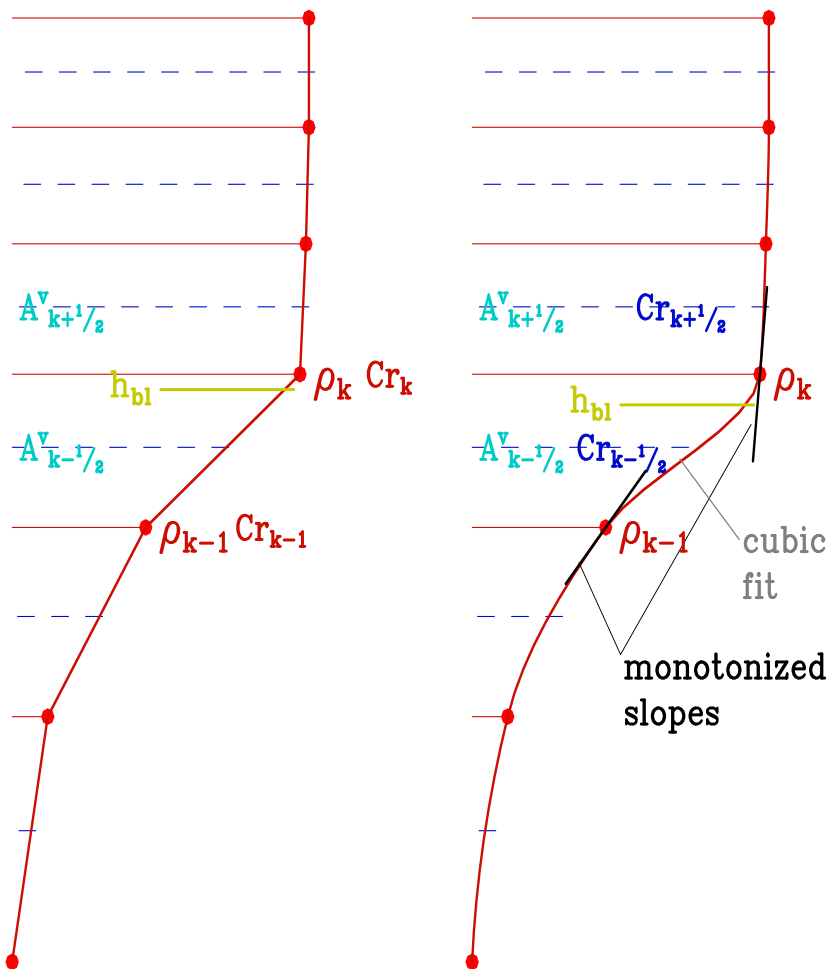
$$A_{k+1/2} \sim \left(z_{k+1/2} - |h_{\text{bl}}| \right)^2$$

near the edge of PBL, hence needs h_{bl} needs accuracy relatively to W -points, while missing ρ -s is more forgiving

- Estimate V_t^2 and $Cr(z)$ at midpoints $z_{k+1/2}$ using monotonized fit for bouyancy (integrated N^2) to estimate its values and derivatives at $z_{k+1/2}$ -interfaces.
- *harmonic* averaging of *adiabatic* differences of density field (the same idea as for computing horizontal pressure gradient)

⇒ unlocking vertical steppiness

⇒ larger variation of PBL, typically shallower in summer



Monotonized reconstruction to compute $V_{t,k+1/2}^2$ and $\rho_{k+1/2}$, but **not** to interpolate Cr to find h_{bl} : because of

$$Cr \sim w_s \sqrt{N^2 - N^2 d}$$

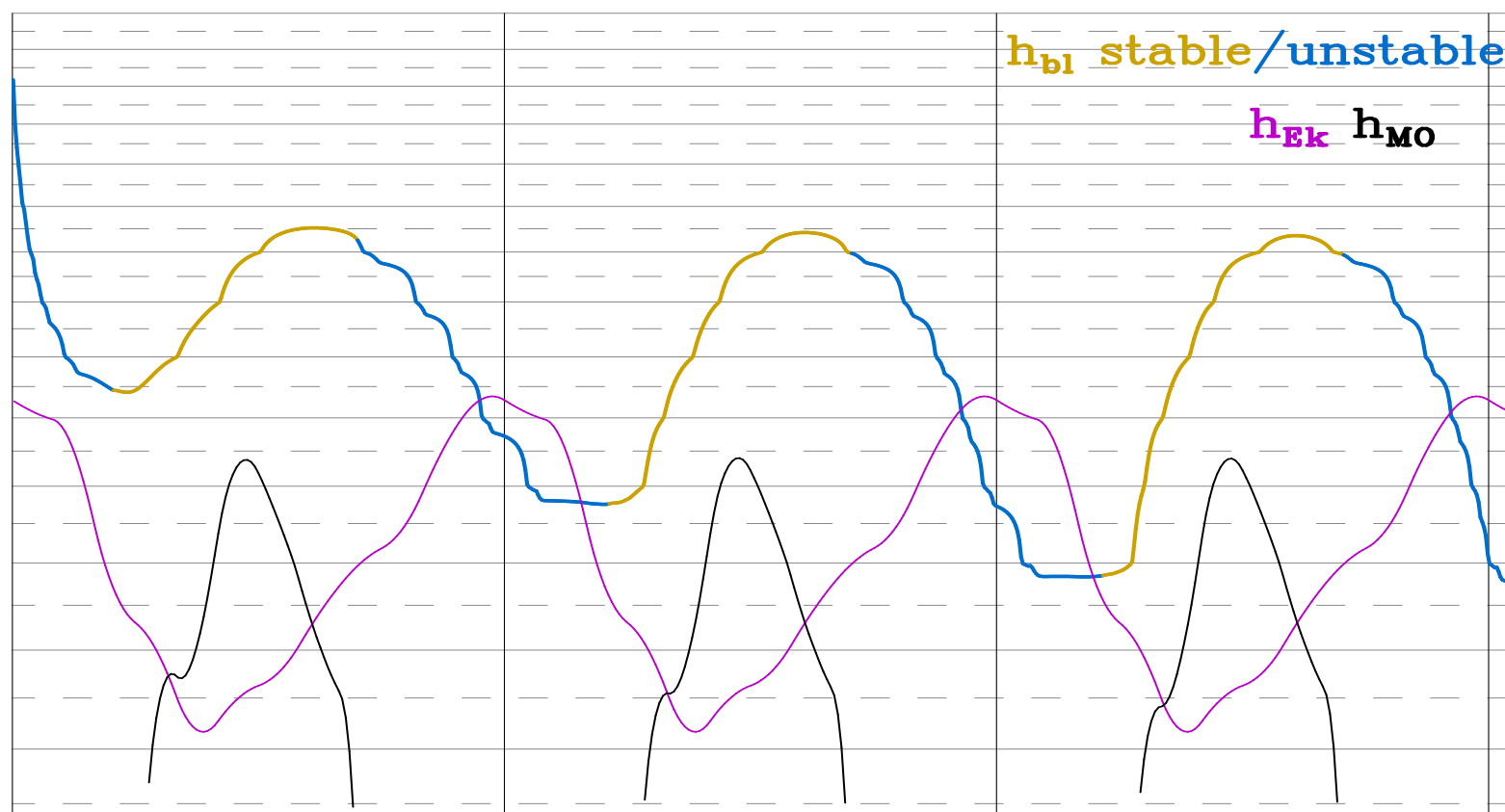
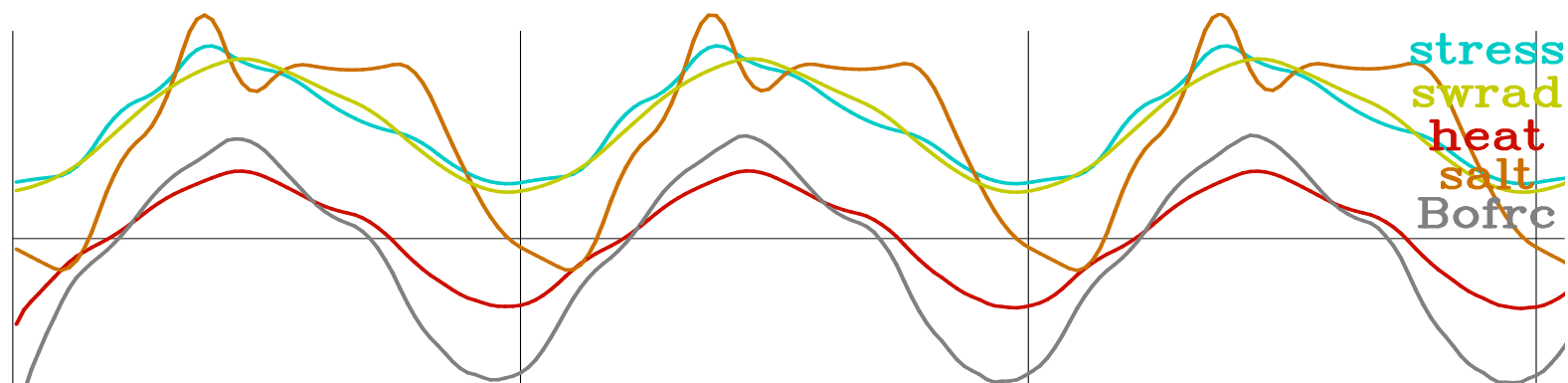
$Cr(z)$ is **not monotonic** near

$$z = -h_{bl}$$

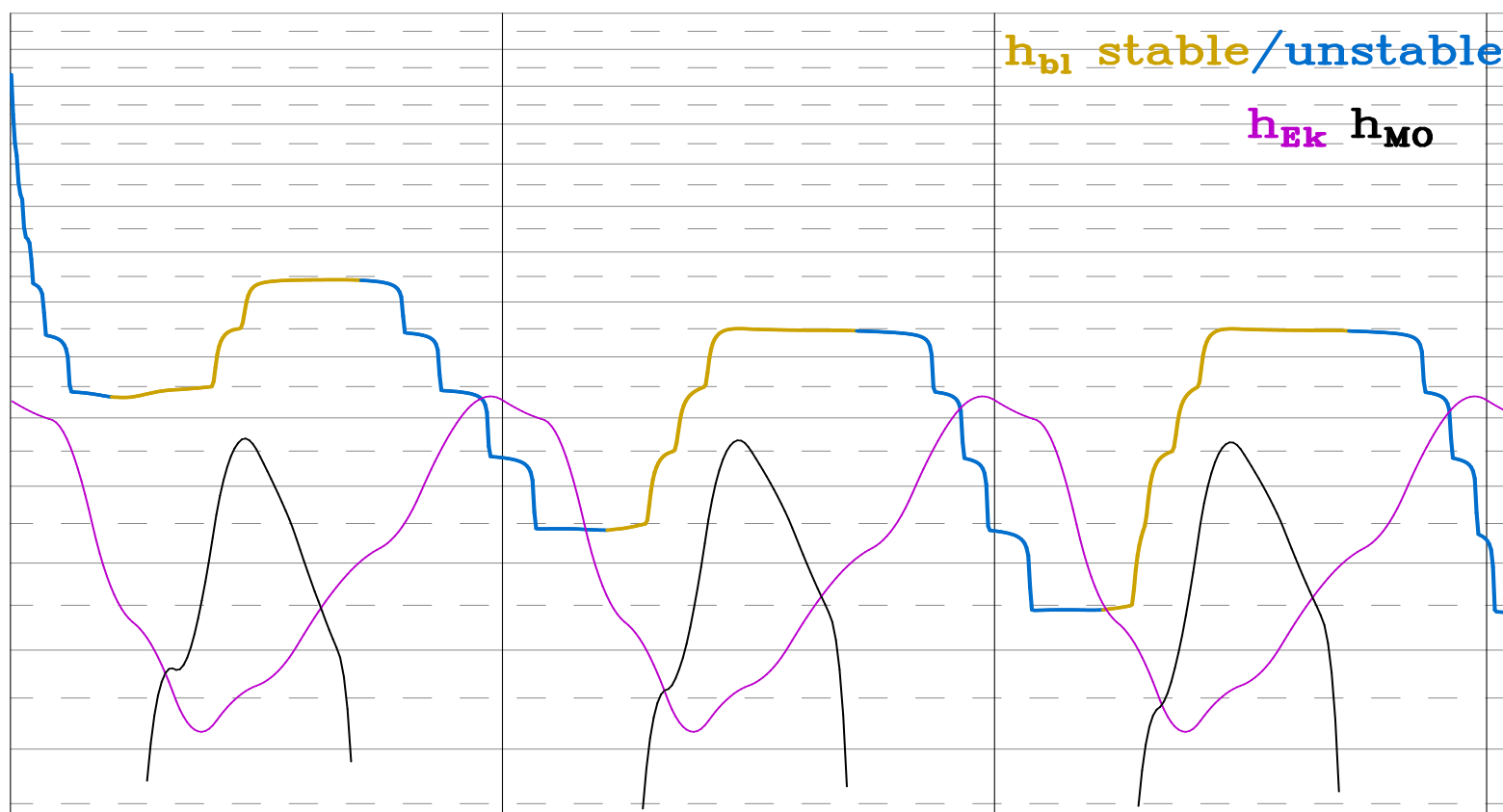
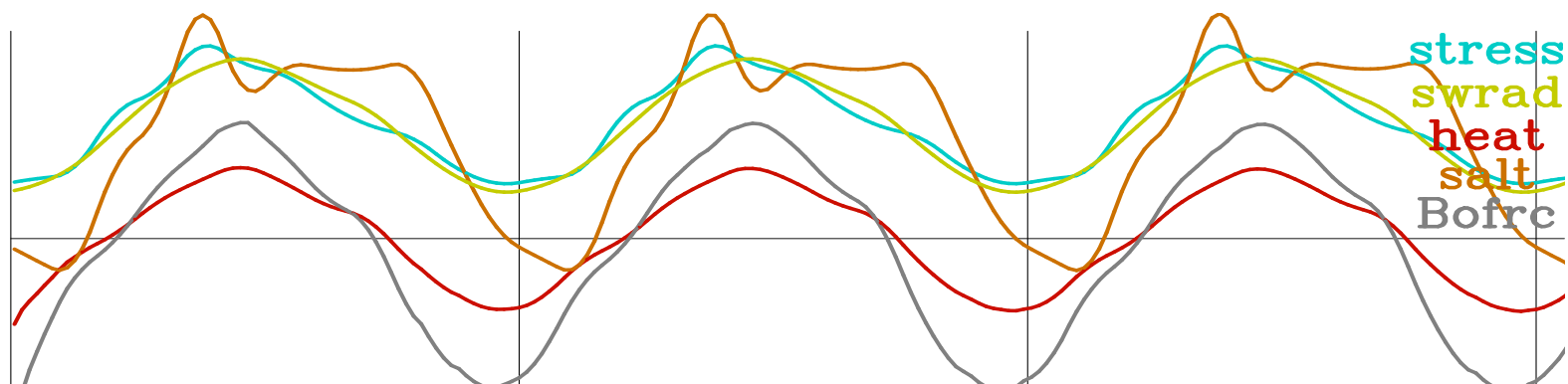
even if $\rho(z)$ and $u, v(z)$ are

\Rightarrow quadratic (cubic) interpolation for Cr is dangerous

Overall this is by far the largest cause of numerical sensitivities in KPP.



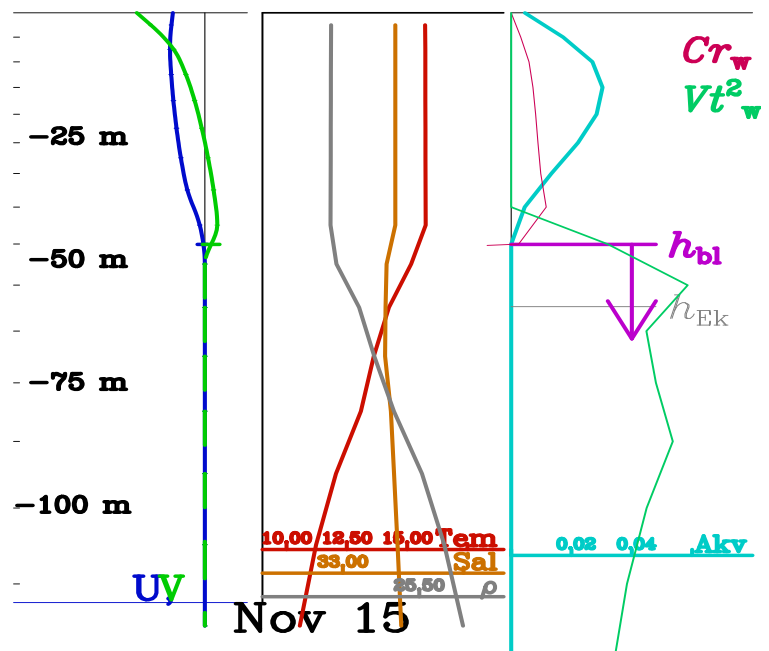
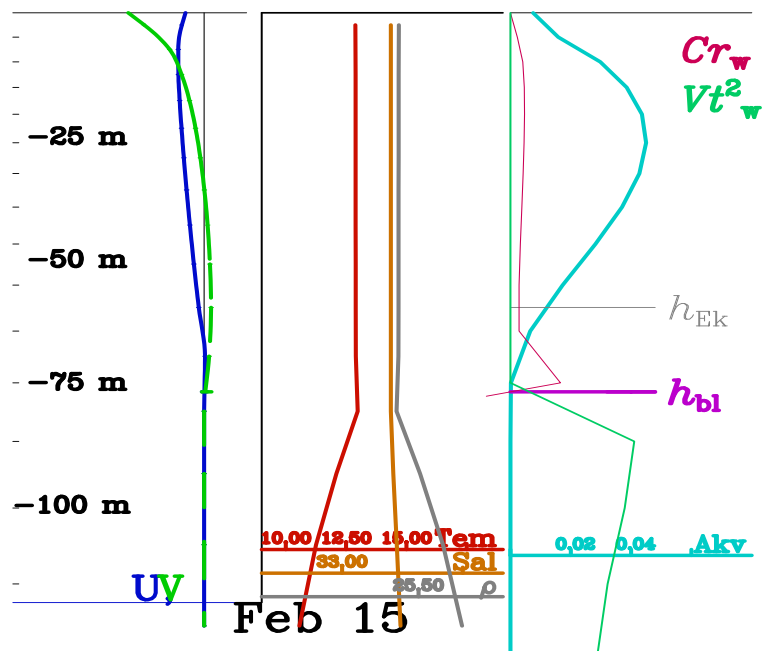
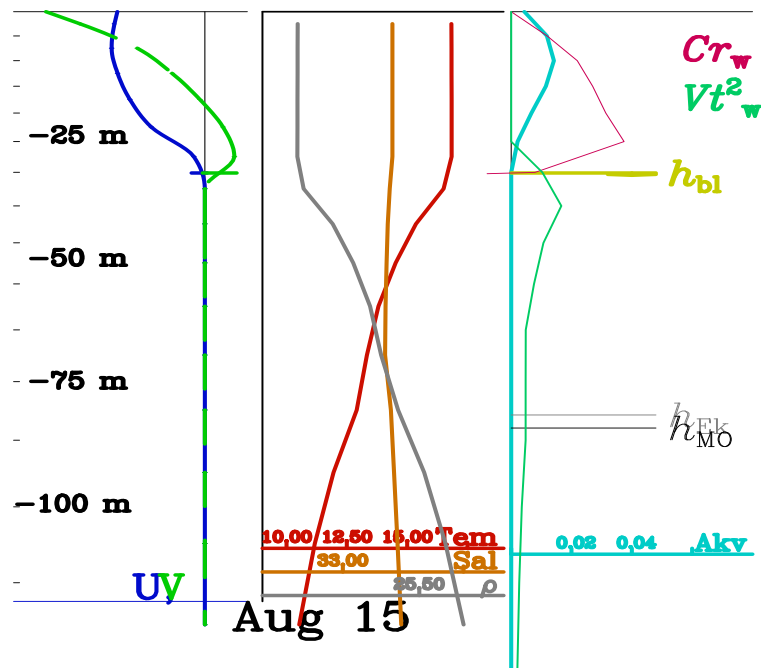
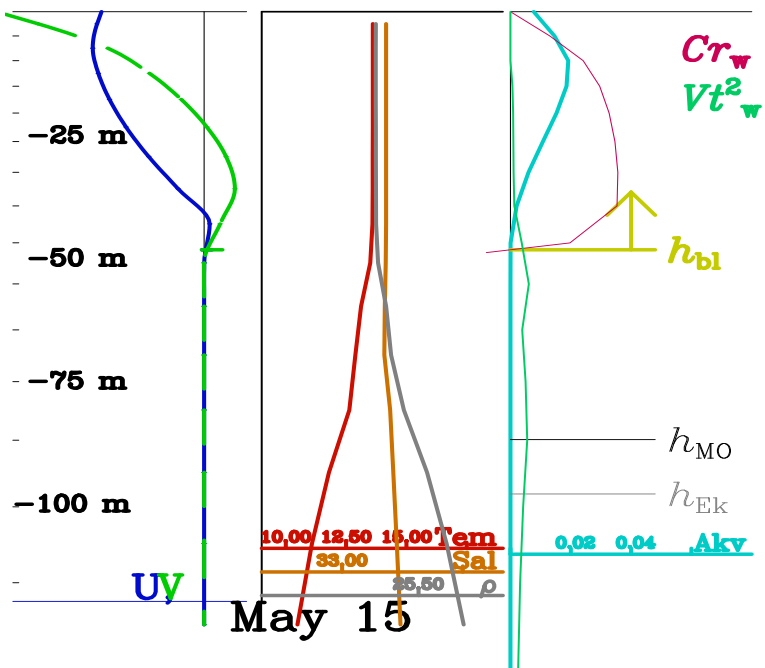
$Cr(z)$ at W -points, $N = 40$

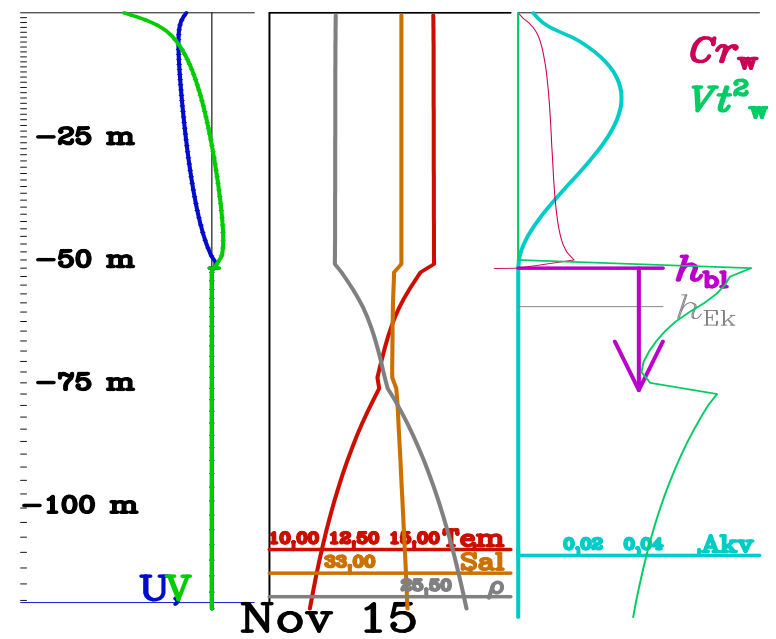
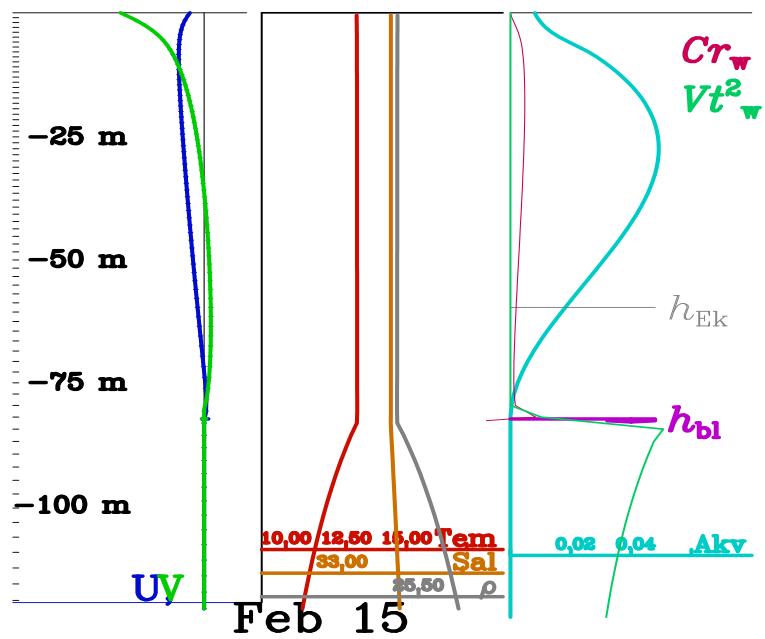
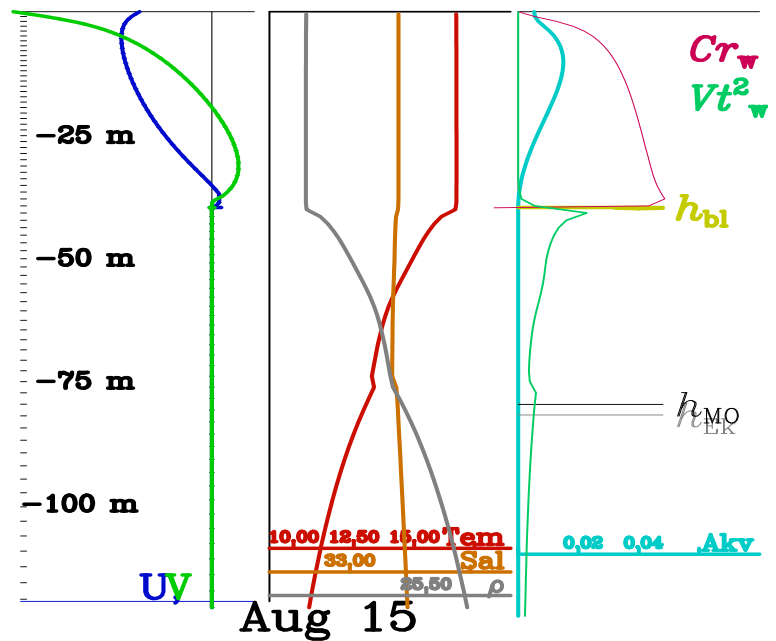
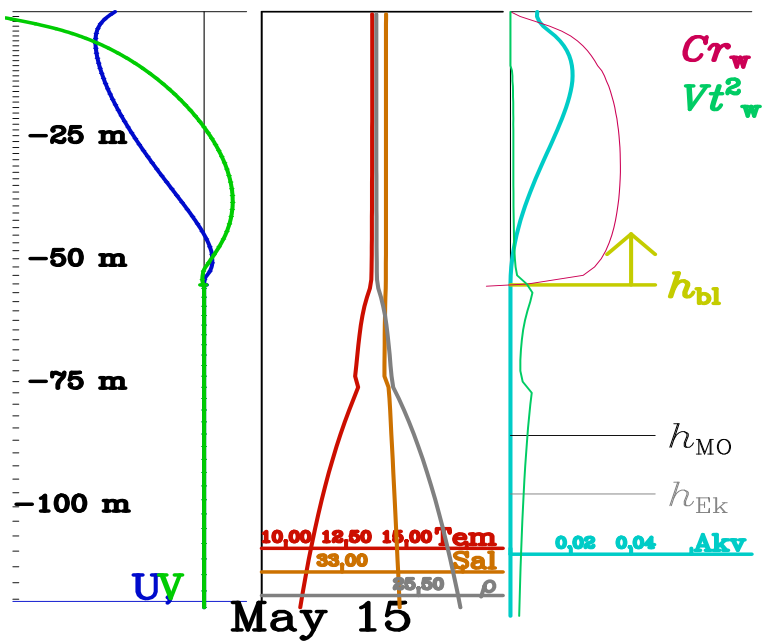


$Cr(z)$ at ρ -points, $N = 40 \Rightarrow$ grid locking

What it all adds up to?

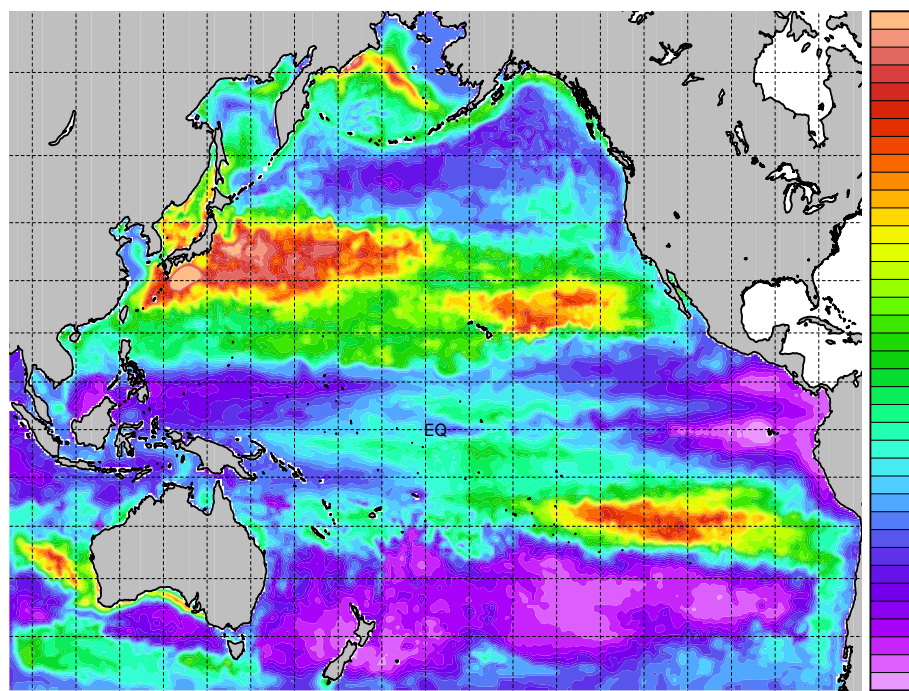
- 1D
- 3D
- comparison with reality



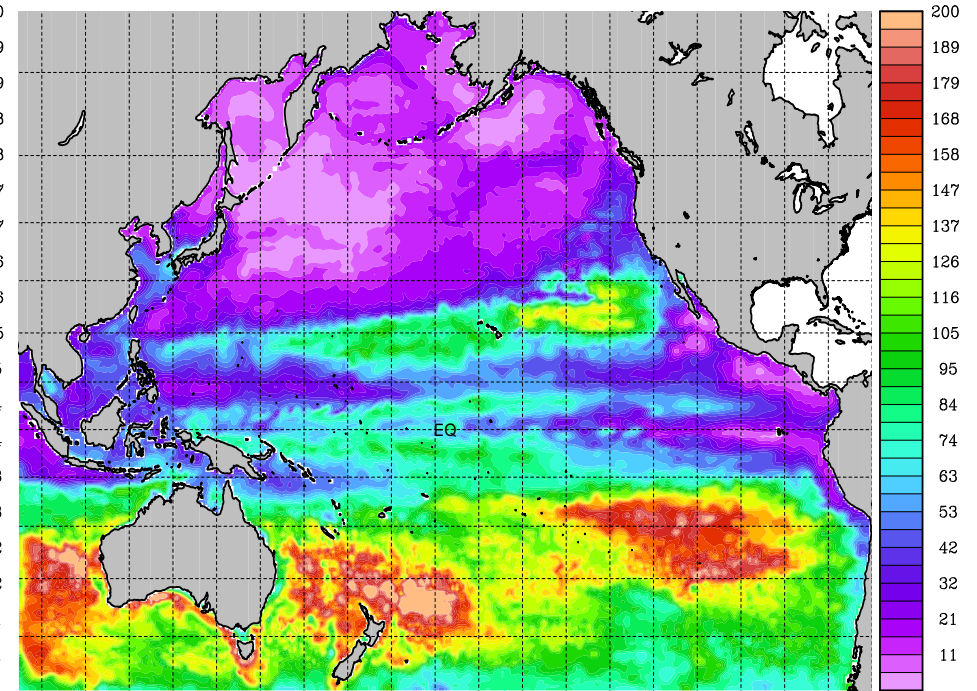


3D Modeling

0.45-degree Pacific Model forced by NCEP winds

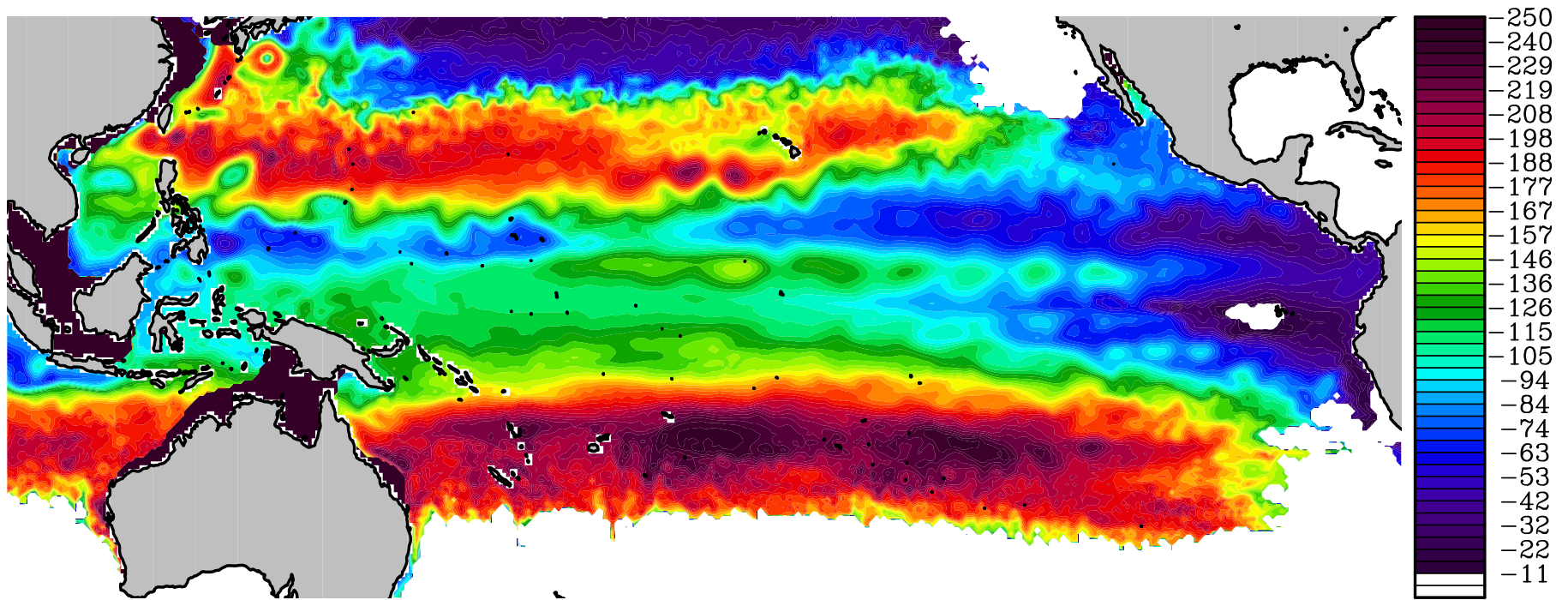


min=0, max=258.8
20 FEB 1995 Depth of Planetary Boundary Layer (m)

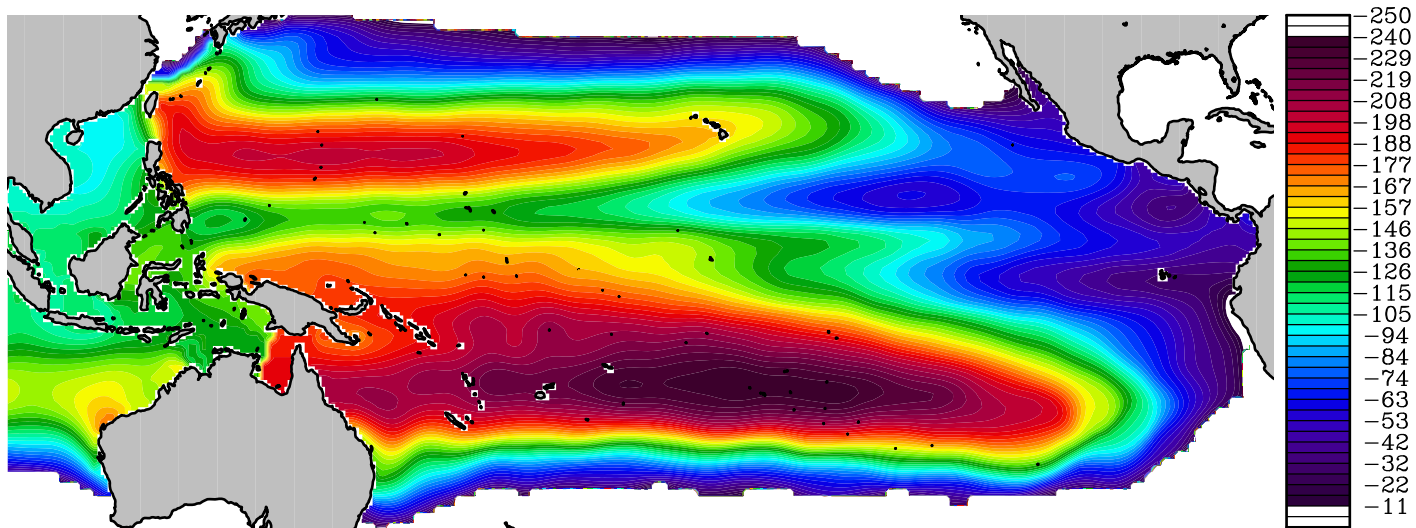


min=0, max=258.5
20 SEP 1995 Depth of Planetary Boundary Layer (m)

seasonal variation of h_{bl} -field



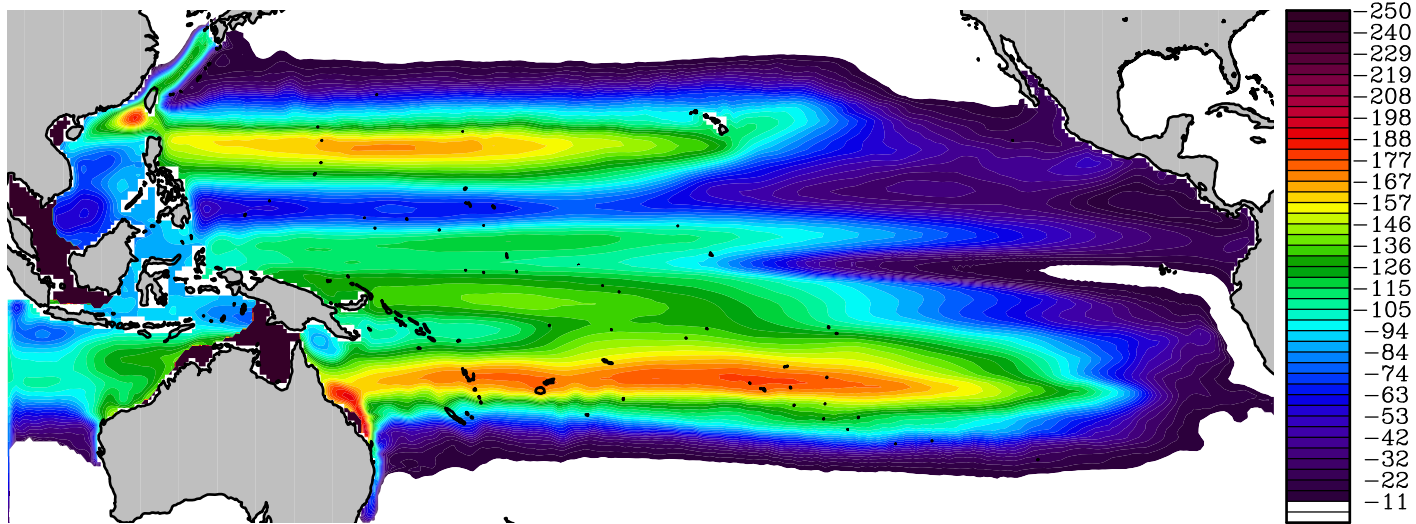
Depth of 20°C isotherm, instantaneous snapshot from a recent 2005 simulation



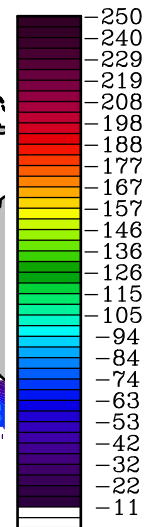
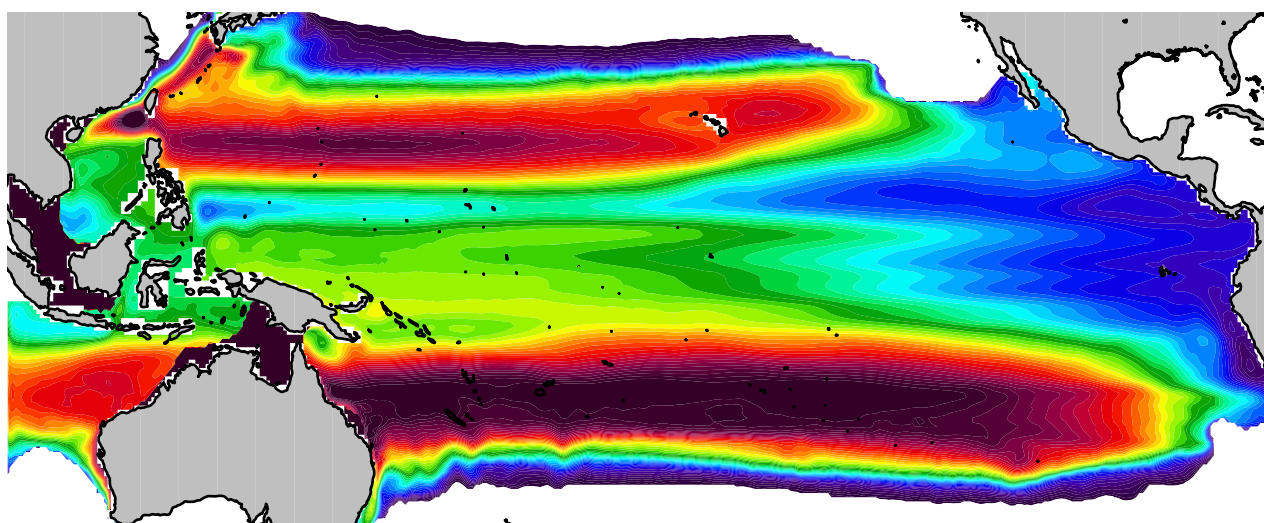
Depth of
20°C isotherm,
10-year
annual mean

Levitus

vs.



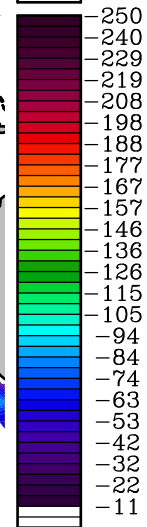
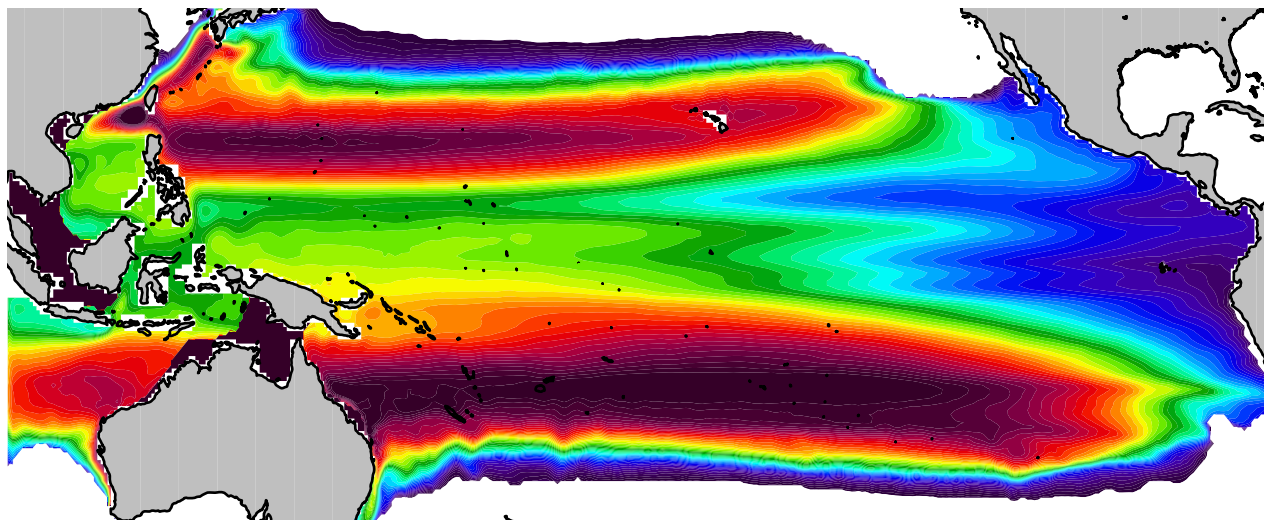
ROMS
with early
2003
baseline
KPP



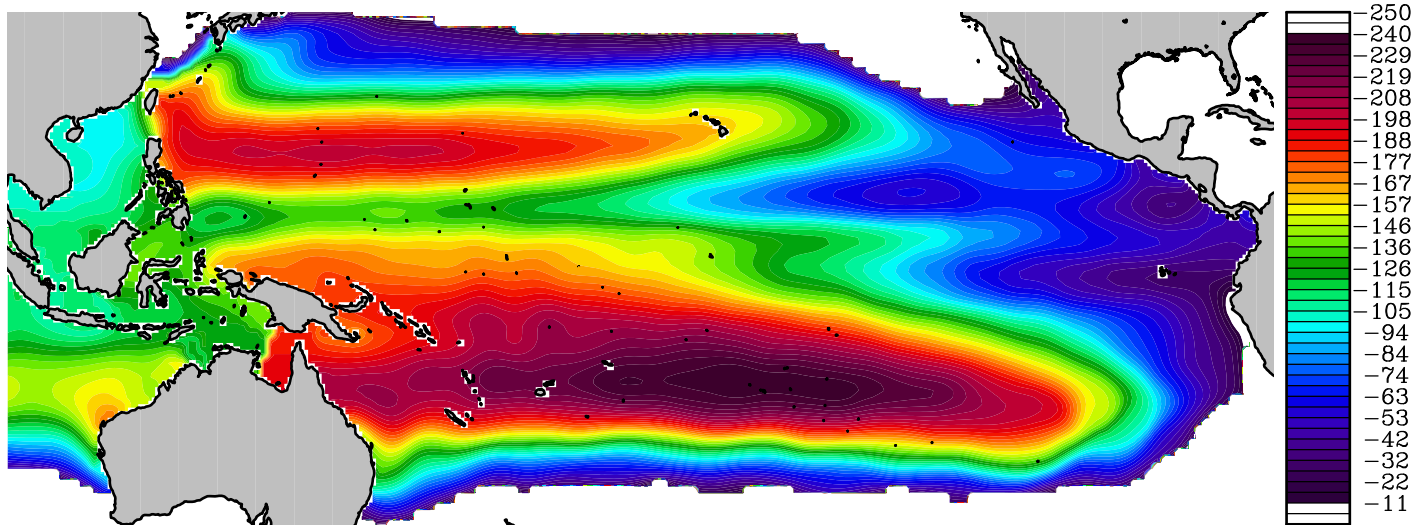
NCEP

vs.

ERS
winds

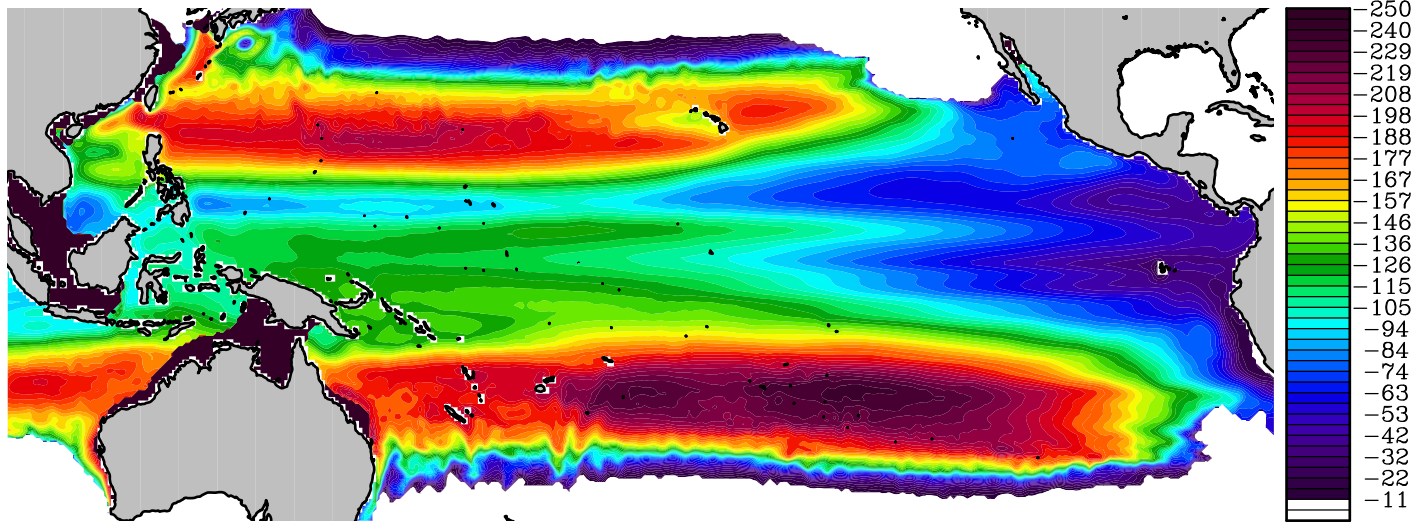


New KPP
in both,
 $Ri_{cr} = 0.45$

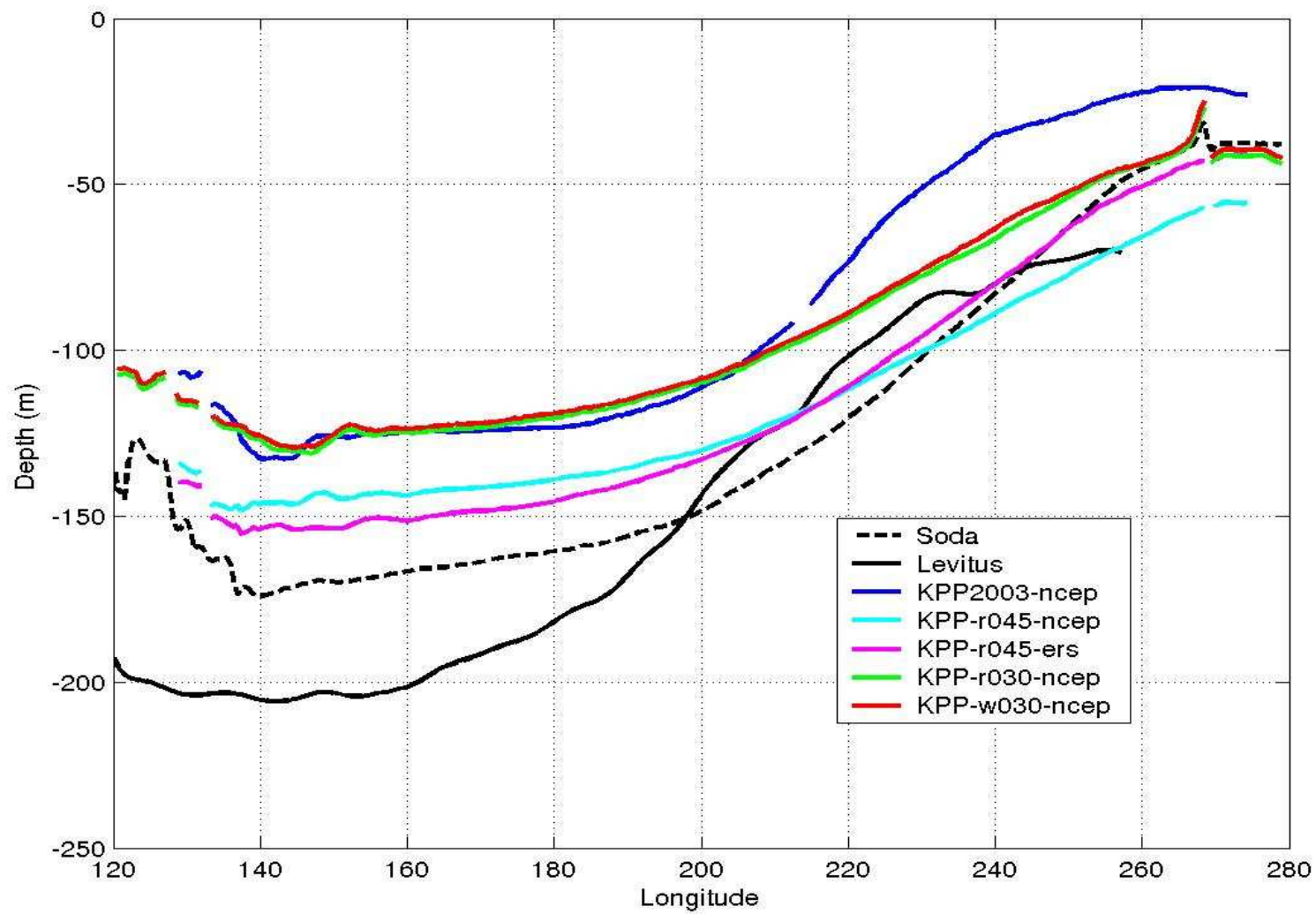


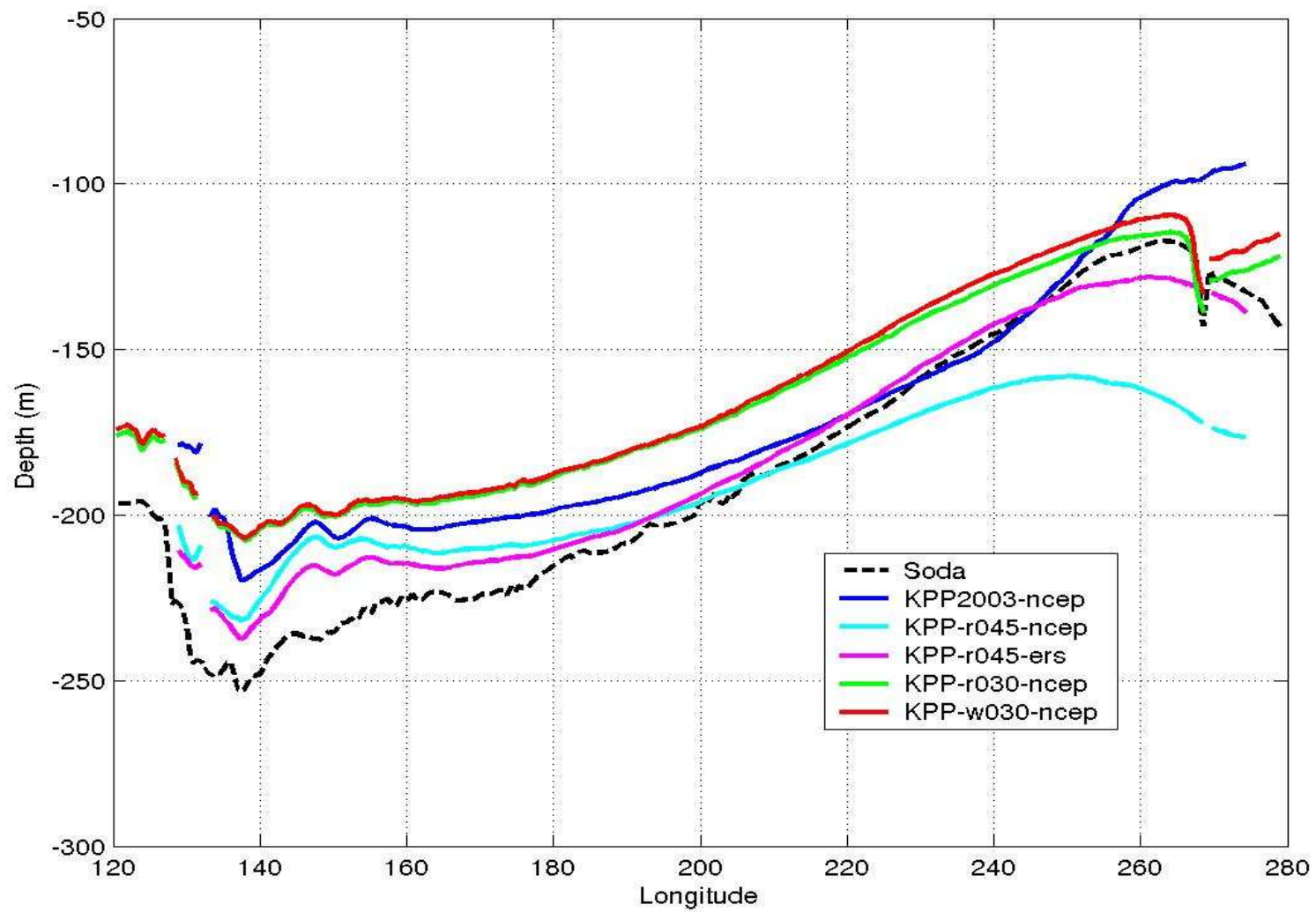
Levitus

vs.



ROMS
with 2005
KPP
still NCEP





US West Coast Model: an Example of Fine Tuning

US West Coast Model, 15 km resolution forced by COAMPS daily winds

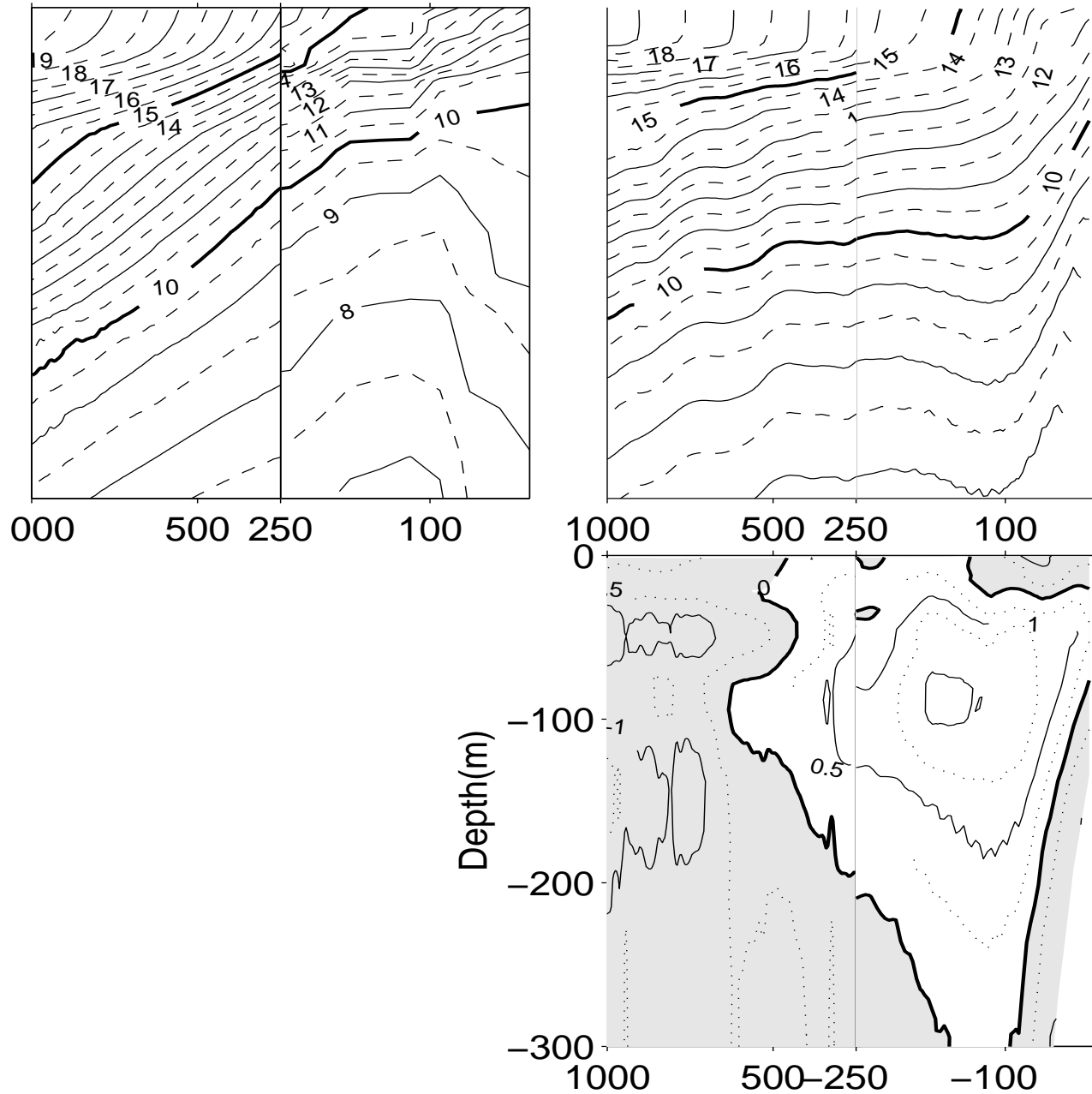
All conditions below are the same, except variations in KPP code.

CalCOFFI (nearshore, $< 250\text{ km}$), and Levitus (beyond that)

showing only summer because this is the worst among 4 seasons

courtesy of Xavier Capet

S3coamps-daily-15km(sum)

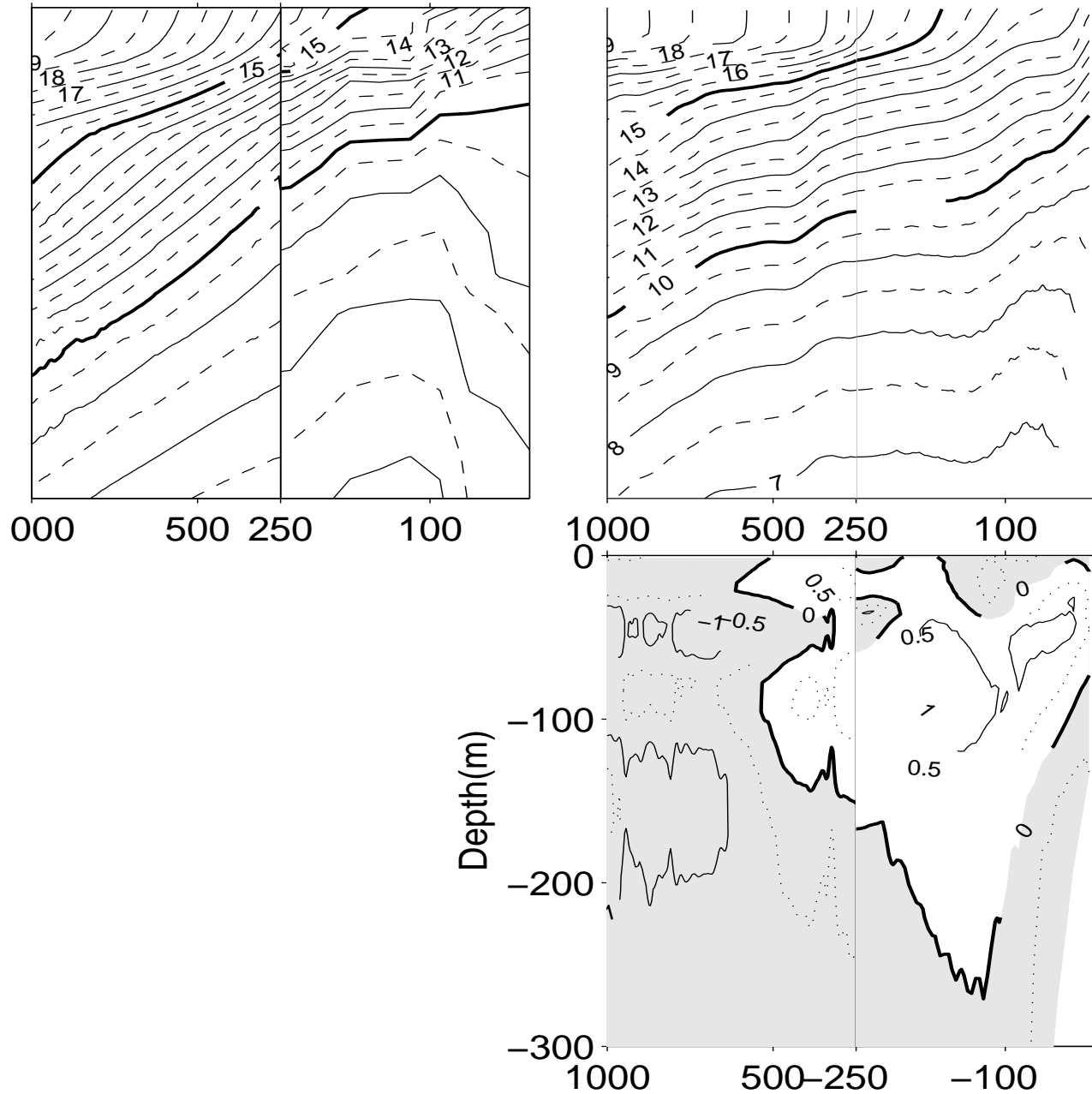


Early 2005 KPP,
 $Ri_{cr} = 0.45$, limiting
 d/L_{MO} for $w_{m,s}$ in
 stable regime

Note slope of
 $10^{\circ}C$ - isotherm

overall $1.5^{\circ}C$
 cold bias offshore
 and $> 2^{\circ}C$ warm
 bias nearshore

S3coamps-shallow-15km(sum)



New 2005 KPP

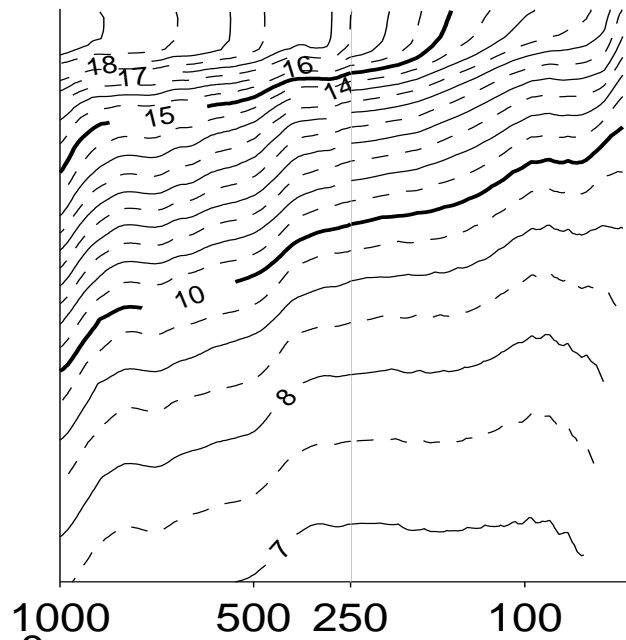
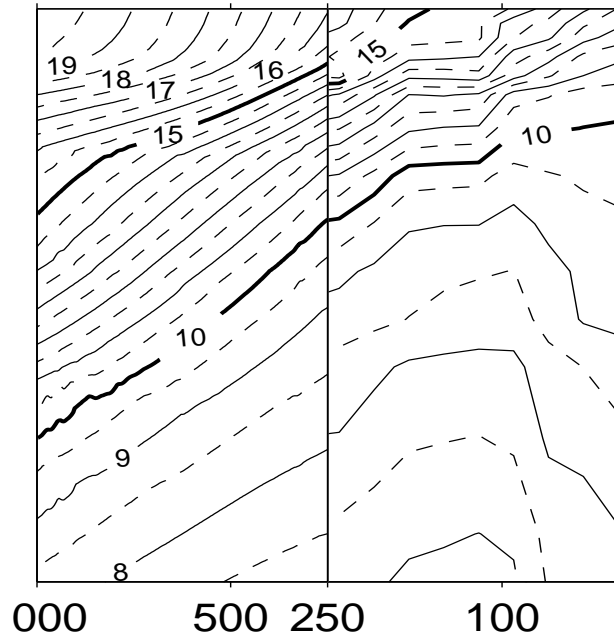
$$Ri_{cr} = 0.45$$

Not limiting d/L_{MO}
in stable regime

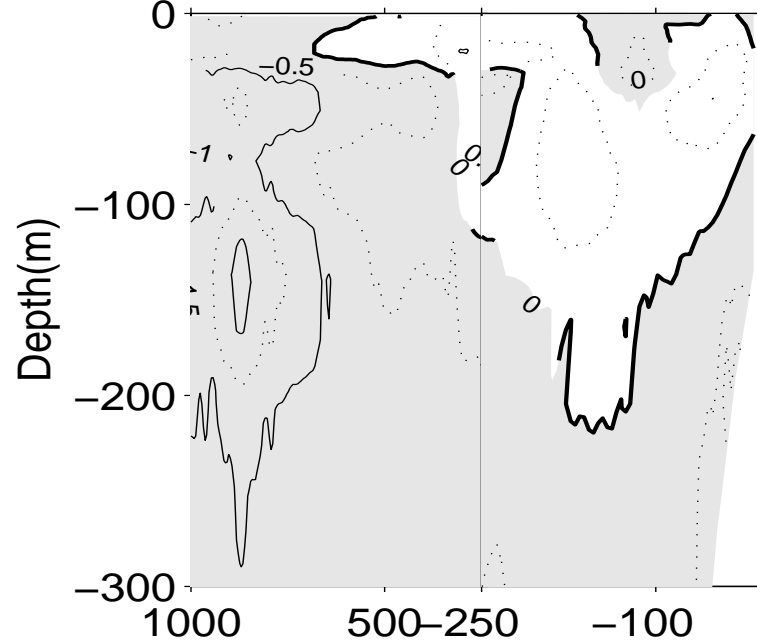
(Fig. 2 of LMD94)

recovered most
of the slope

S3coamps-daily_n kkpr-luo-15km(sum)

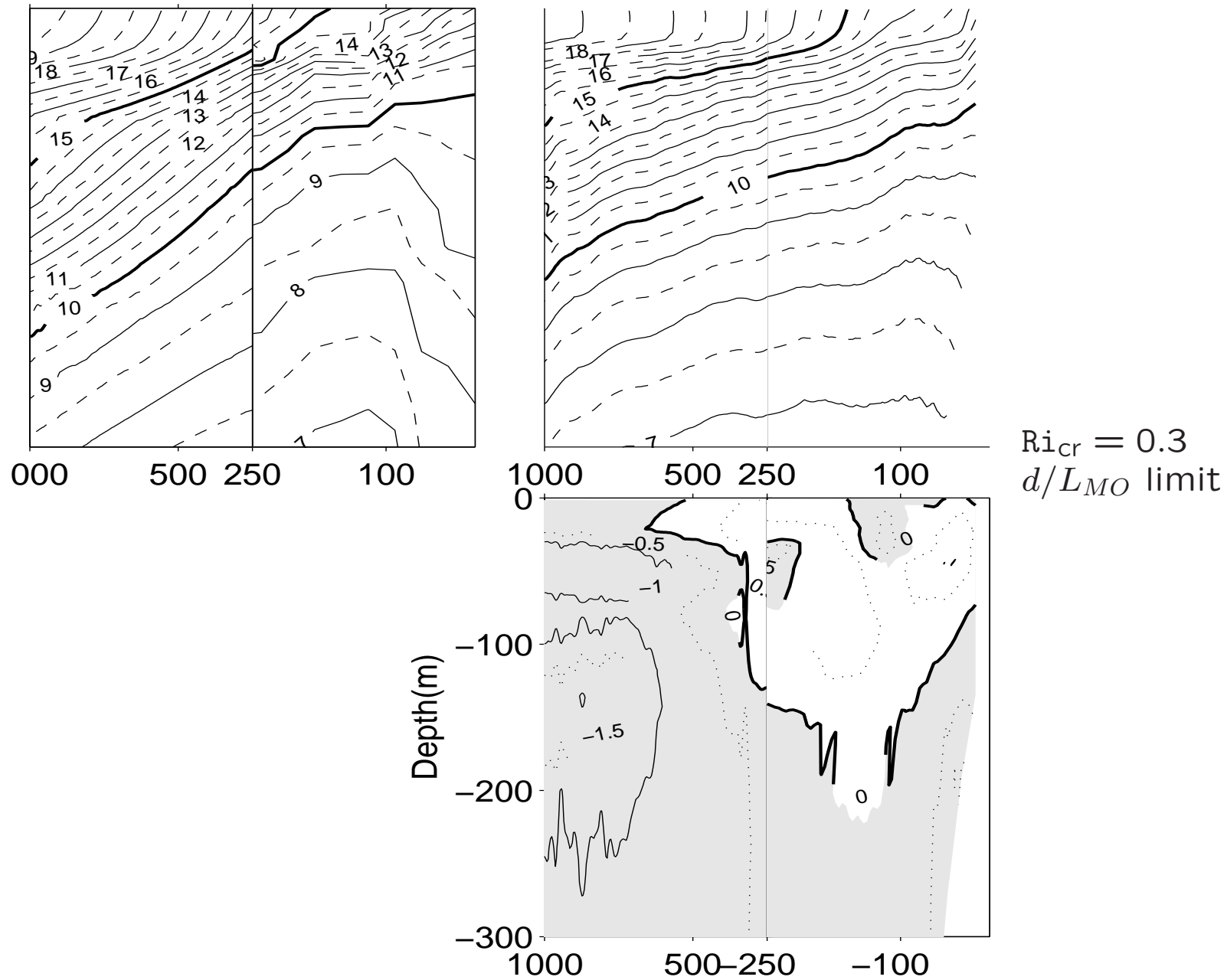


$Ri_{cr} = 0.3$
No d/L_{MO} limit



shallow-shore bias off-shore

S3coamps-daily_n kkpr-15km(sum)



Summary

- Accepted most (not all) updates from W. Large and G. Danabasoglu
- **integral Cr -based search for h_{bl}**
- kernel $\mathcal{K}(\sigma)$ to account for surface sublayer \Rightarrow convergence
- replaced h_{EK} limit with new treatment of Ekman boundary layer
- Corrected Monin-Obukhov limitation algorithm.
Subsequently eliminated it altogether
- Do not limit $\zeta = d/L_{MO}$ in $w_{m,s}$ computation in stable regime
- Changed non-local flux to ensure its continuity at h_{bl}
- Surface wave mixing: $A_k \rightarrow$ finite limit at $z \rightarrow \zeta$
- **Significantly reduced resolution drift**
- **"shallow bias" is now under control**
- Changes for free-surface compatibility with free surface of ROMS
(fixed blow-ups in shallow regions)
- code rewritten from scratch (yet, again) for efficiency

Lessons learned

- 1D model is very useful for process studies and numerical algorithm verification, but **not for parameter tuning against real-world data**
- Boundary layer depth h_{bl} , as diagnosed by KPP, is not directly comparable to mixed layer empirically derived from data (cf., Levitus, $0.8^\circ C$ -rule, etc). Compare primary field [T,S] field structure instead.
- 3D simulations show significantly less sensitivity to KPP algorithm and parameter settings than 1D, yet the quantitative differences are comparable to that of different forcing products